
High-Entropy Alloy CoCrFeMnNi Produced by Powder Metallurgy

Nadine Eißmann, Burghardt Klöden, Thomas Weißgärber, Bernd Kieback

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Content

1. Fundamentals and Motivation
2. Powder Manufacturing
3. Pressureless Sintering (MIM)
4. Spark Plasma Sintering
5. Electron Beam Melting
6. Comparison Production Methods
7. Summary and Outlook

1. Fundamentals and Motivation

High-Entropy Alloys (HEAs):

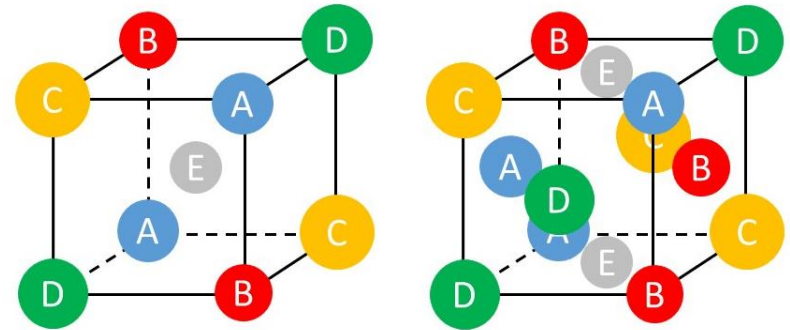
- 5 principal elements, each 5 till 35 at%
- Minor elements, below 5 at%

Properties

- Simple solid solution phases
- High hardness and strength
- Good thermal stability
- Excellent corrosion, wear and oxidation resistance

Applications

- Tools, molds, dies, mechanical and furnace parts
- Anticorrosive high-strength materials in chemical plants, and IC foundries
- Functional coatings and diffusion barriers



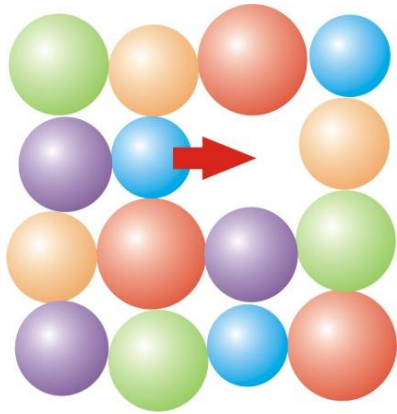
Crystal structure of HEAs

1. Fundamentals and Motivation

Core Effects in High-Entropy Alloys

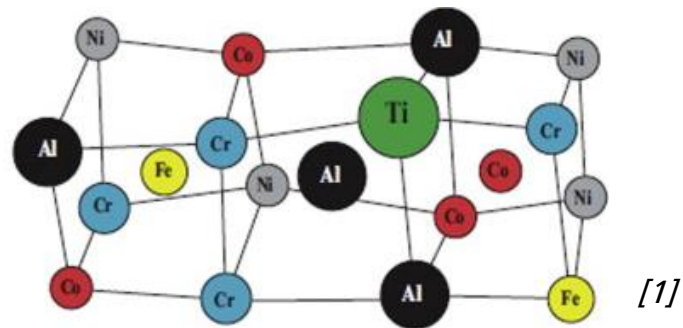
High-Entropy Effect

$$\Delta S_{mix} = -R \sum_{i=1}^n X_i \ln X_i$$



Sluggish Diffusion Effect

Lattice Distortion Effect



1. Fundamentals and Motivation

Core Effects - High-Entropy Effect

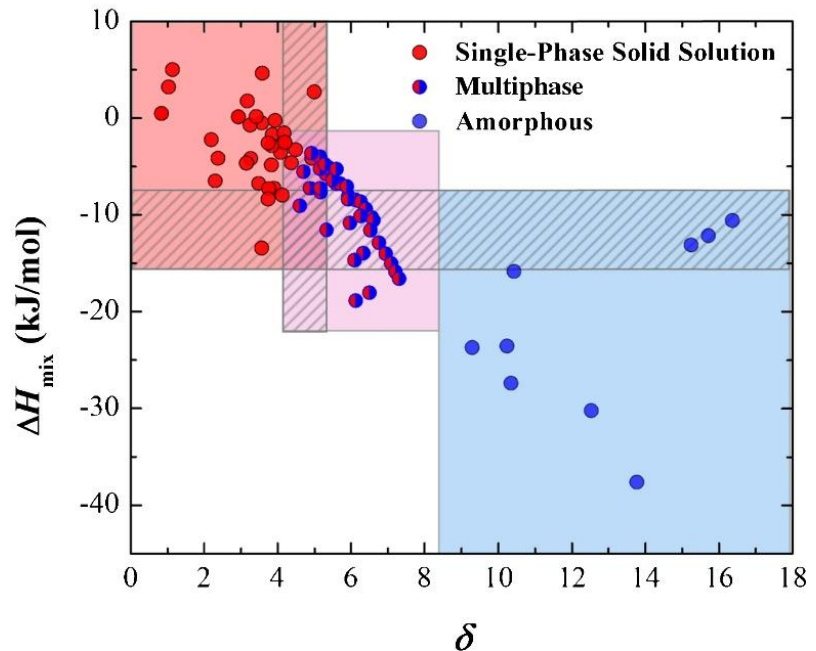
Assumption:

- Entropy of mixing ΔS_{mix} stabilises solid solution phases
⇒ Origin of the name

Experimental results:

- Phase analysis shows also amorphous and intermetallic phases
- Entropy of mixing not sufficient for stability of HEAs
⇒ Further thermodynamic parameters (enthalpy of mixing ΔH_{mix} , atomic size different δ , ...) under intense investigation

$$\Delta S_{mix} = -R \sum_{i=1}^n X_i \ln X_i$$



Influence of thermodynamic parameters on resulting microstructure [2]

1. Fundamentals and Motivation

Core Effects - Sluggish Diffusion Effect

Assumption:

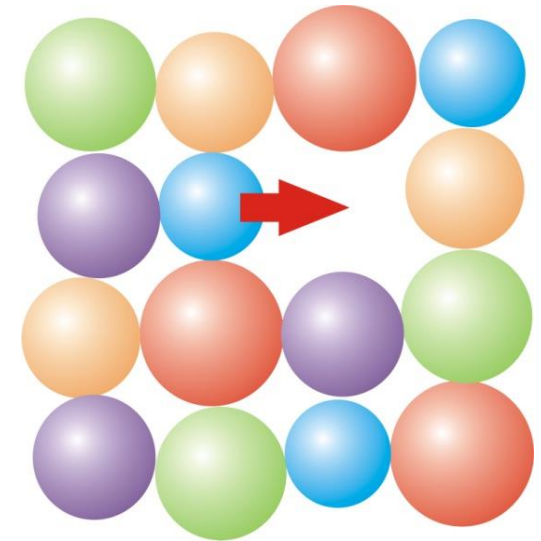
- Sluggish diffusion in HEAs
- *Mobility of atoms: HEAs < steel < raw metals*

Experimental results:

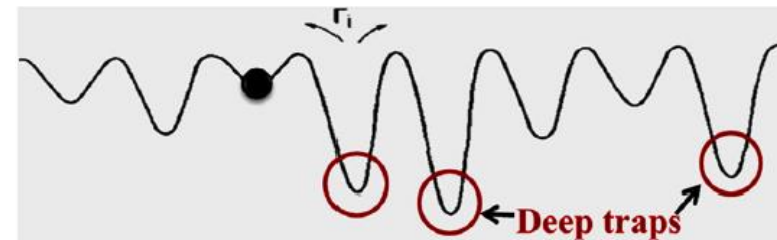
- Different bonding configuration dependent on lattice site
- *Lattice potential energy* LPE varies depending on the lattice site
 - ⇒ LPE low → traps

Consequences:

- Influence on all diffusion-controlled processes
 - ⇒ Metastable phases
 - ⇒ Slow grain growth
 - ⇒ Nano precipitations



Diffusion in HEAs



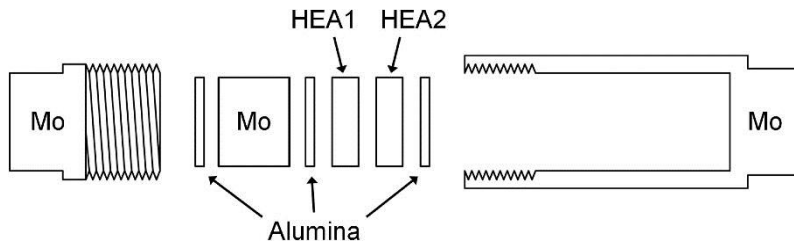
Fluctuation of LPE for diffusion path of atoms in HEAs [3]

1. Fundamentals and Motivation

Core Effects - Sluggish Diffusion Effect

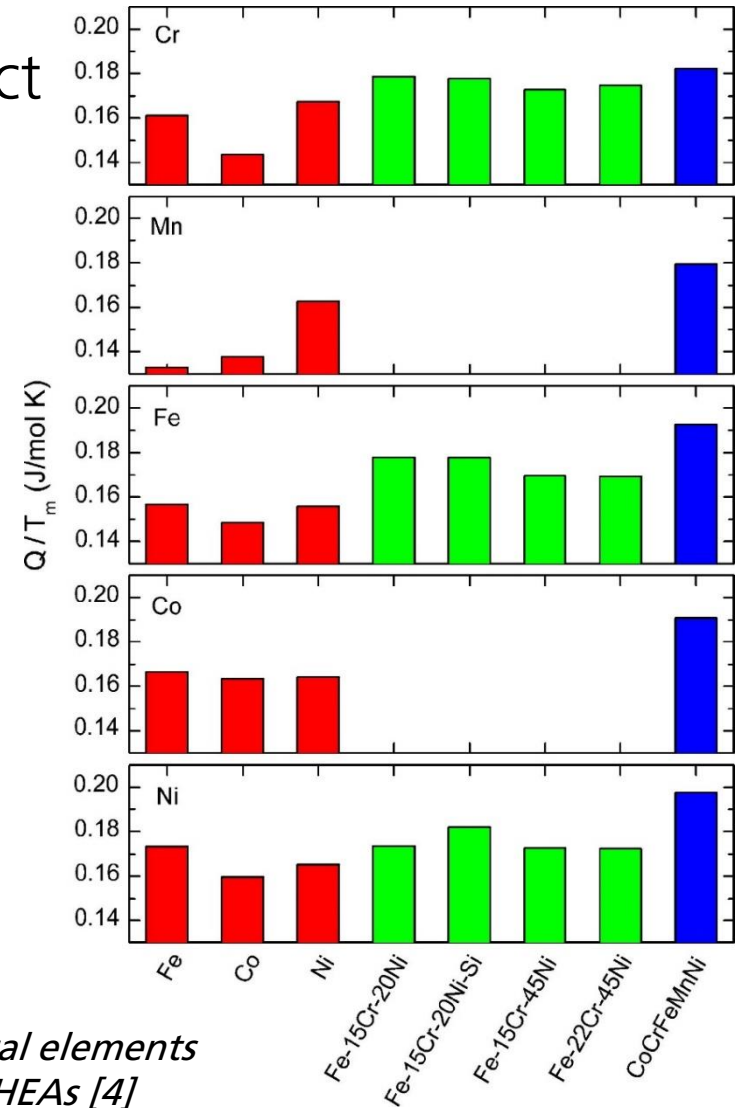
⇒ First diffusion research by *Tsai et al.* (2013) for CoCrFeMn_{0.5}Ni HEA

$$D = D_0 e^{-\frac{Q}{RT}}$$



Schematic diagram showing the assembly of the diffusion couples (900, 950, 1000 and 1050°C) [4]

Activation energy for several elements in conventional alloys and HEAs [4]



1. Fundamentals and Motivation

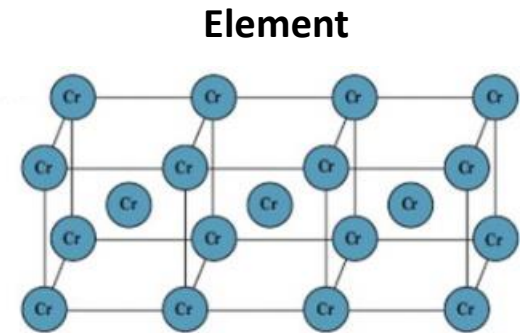
Core Effects - Lattice Distortion Effect

Assumption:

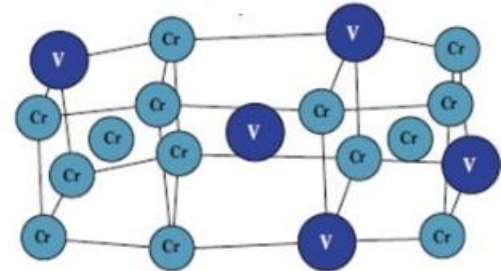
- Varying atomic sizes cause severe distortions
- No difference between matrix and solute atoms

Consequences: Influence on properties

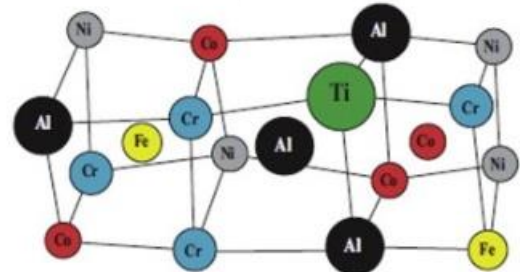
- Impeding of dislocation motion
 - ⇒ Solid solution strengthening
 - High hardness
 - E.g.: MoNbTaVW → HV 530
- Electron and phonon scattering
 - ⇒ Electrical and thermal conductivity are low



Conventional alloy



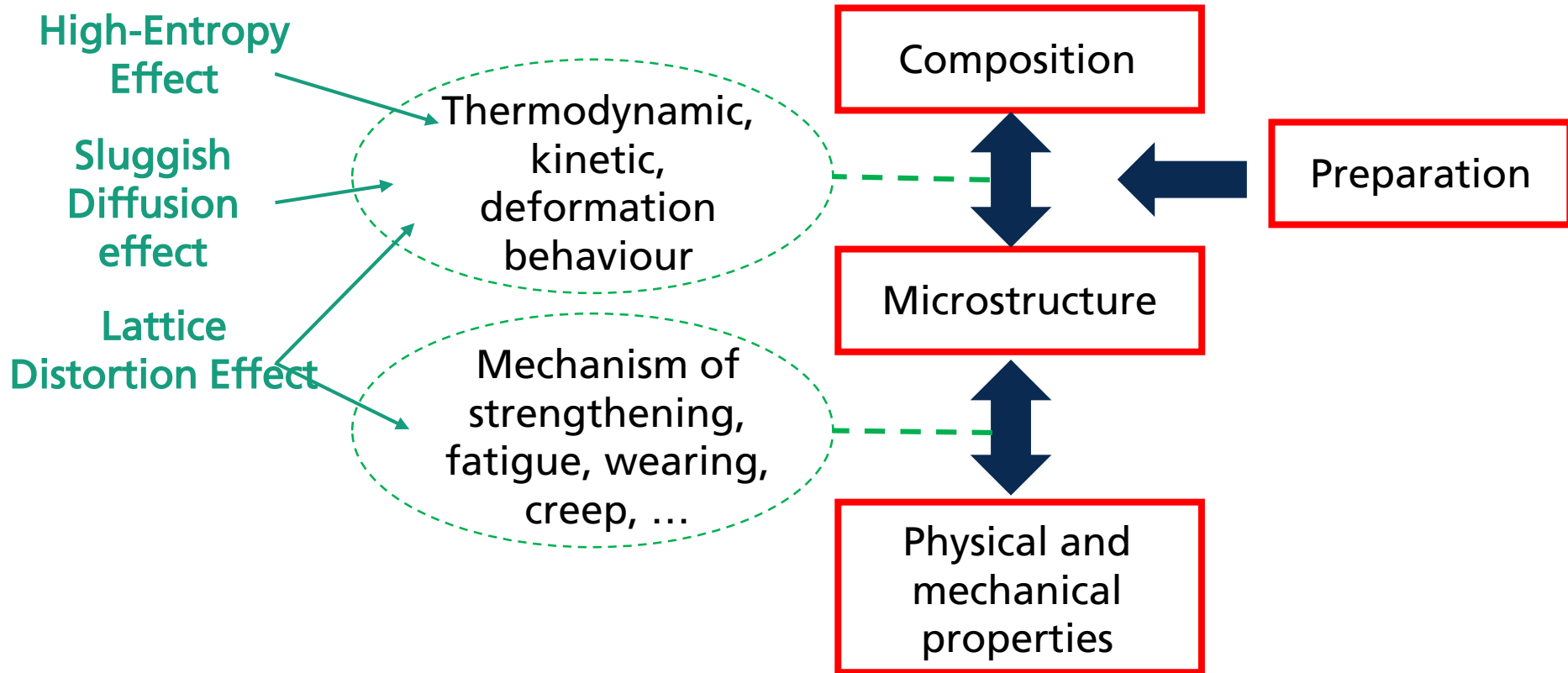
HEA



Lattice distortion in elements, conventional alloys and HEAs [1]

1. Fundamentals and Motivation

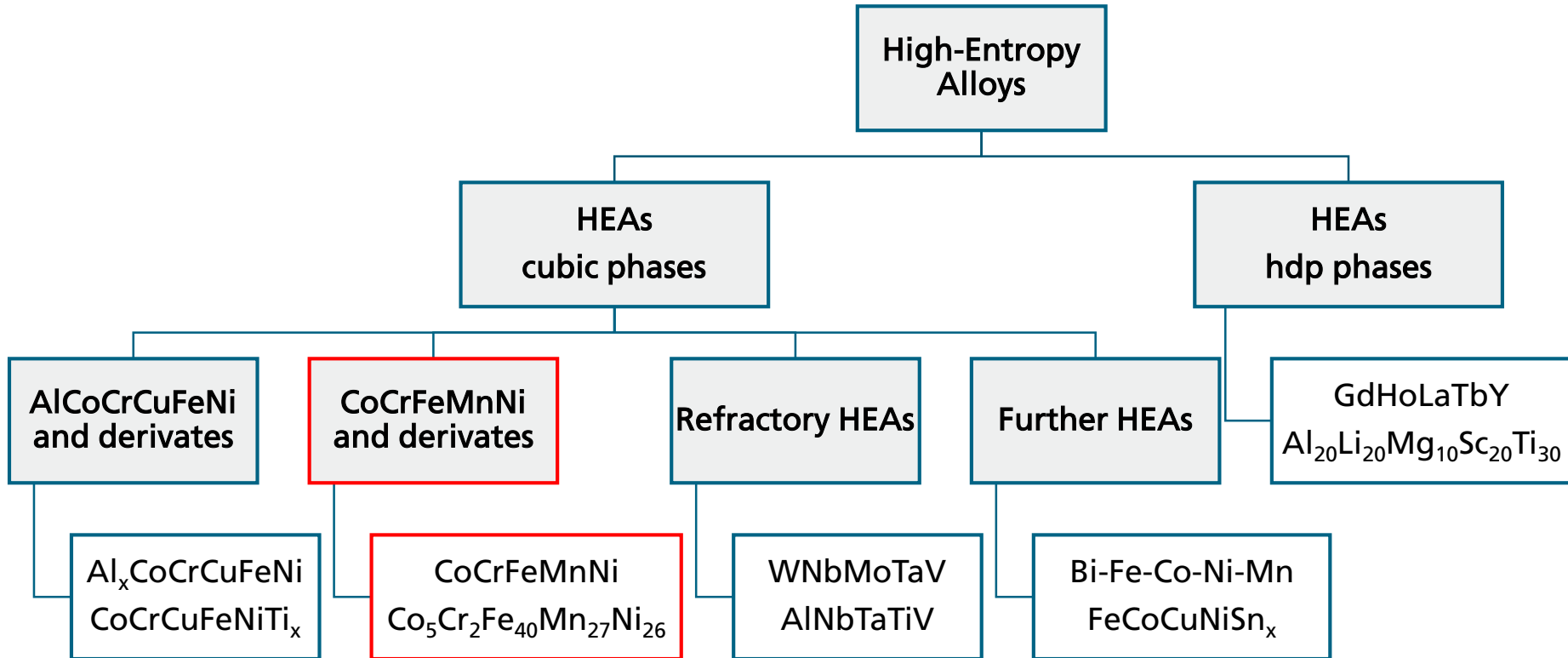
Core Effects - Summary



[3]

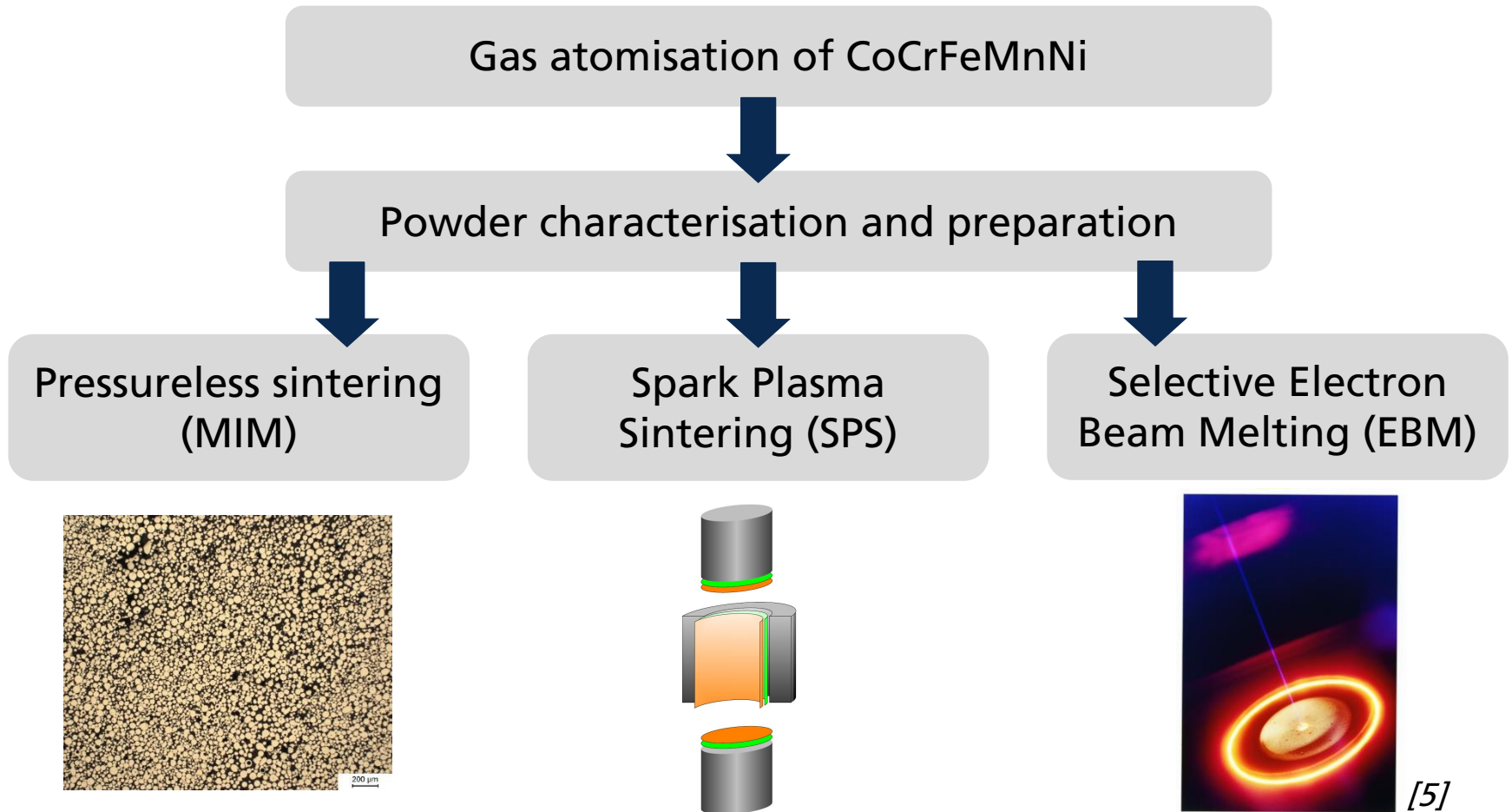
1. Fundamentals and Motivation

World of High-Entropy Alloys



1. Fundamentals and Motivation

Powder Metallurgical Preparation of CoCrFeMnNi

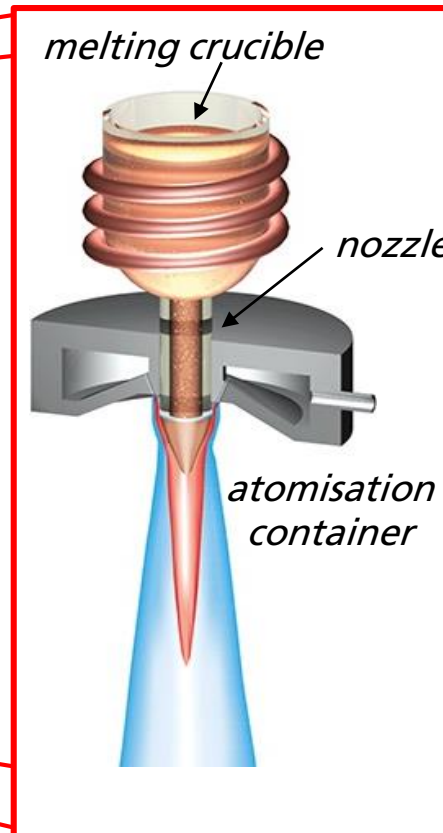


2. Powder Manufacturing

Argon Gas Atomisation



Atomisation facility [6]

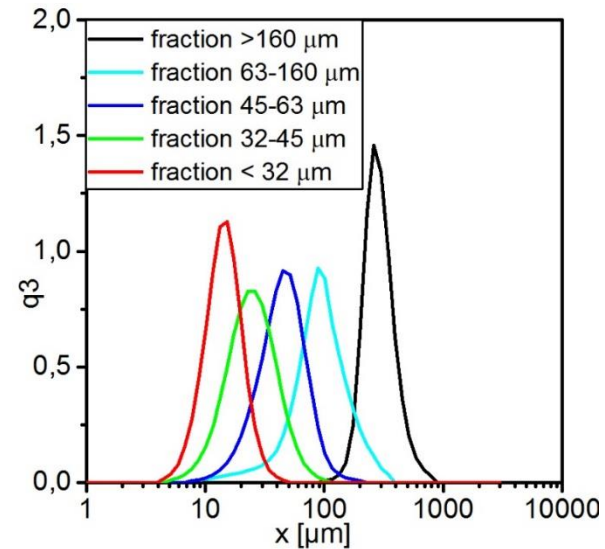
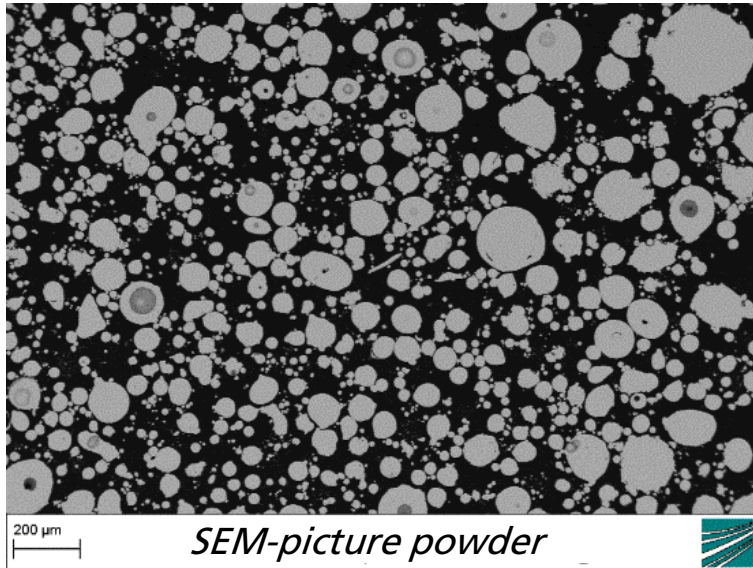


Atomisation principle [7]

- Argon gas atomisation (*Fraunhofer UMSICHT*)
- Starting material: Mixture of raw elements
- Atomising of melt by compressed argon

2. Powder Manufacturing

Powder Characterisation of CoCrFeMnNi



Particle size distribution after sieving process

EDS-analysis powder

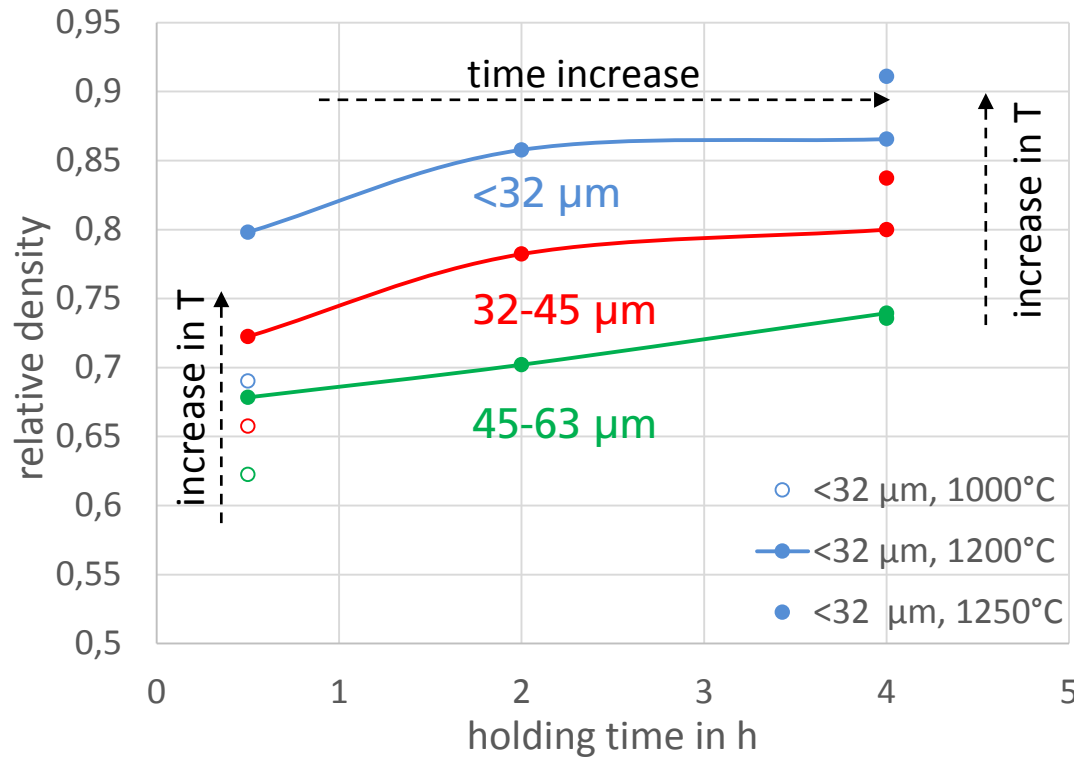
| at-% | Cr | Mn | Fe | Co | Ni |
|---------------|-----------|-----------|-----------|-----------|-----------|
| Pulver | 20,2 | 20,2 | 19,7 | 19,8 | 20,1 |
| He et al. [5] | 21,3 | 20,7 | 19,4 | 19,3 | 19,3 |
| SOLL | 20 | 20 | 20 | 20 | 20 |

CoCrFeMnNi powder

- Single phase microstructure
- Ideal composition

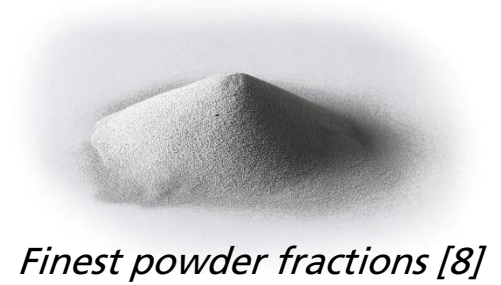
3. Pressureless Sintering (MIM)

Sintering of Loose Powders



Influence of sintering time on density (1200°C)

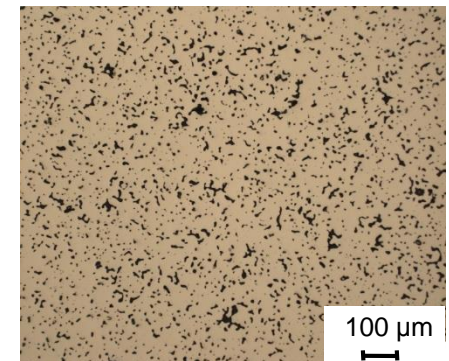
- Increase in sintering time followed by an increase in relative density ρ/ρ_{theo}
- Densities $\rho/\rho_{theo} > 85\%$ for finest powder



Finest powder fractions [8]



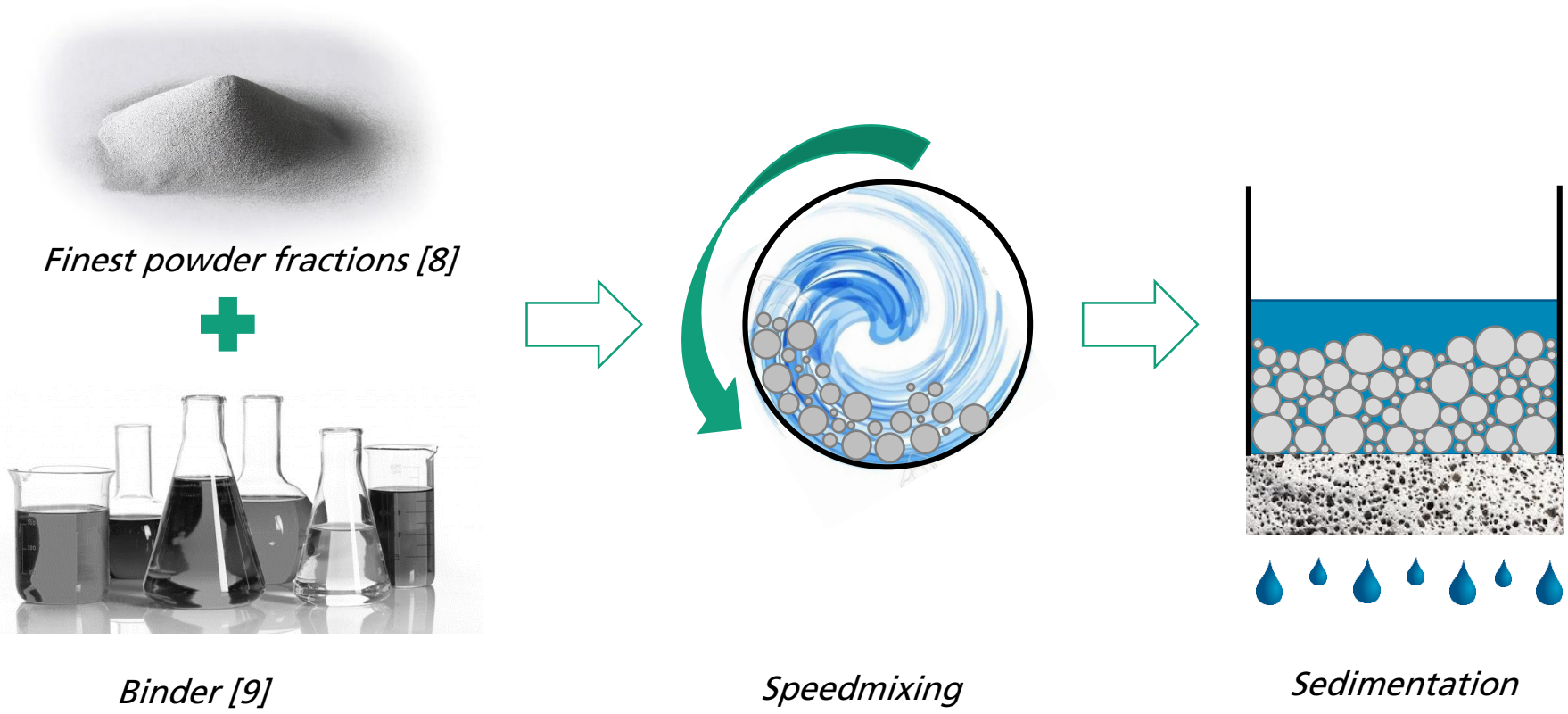
Heat treatment



Resulting microstructure

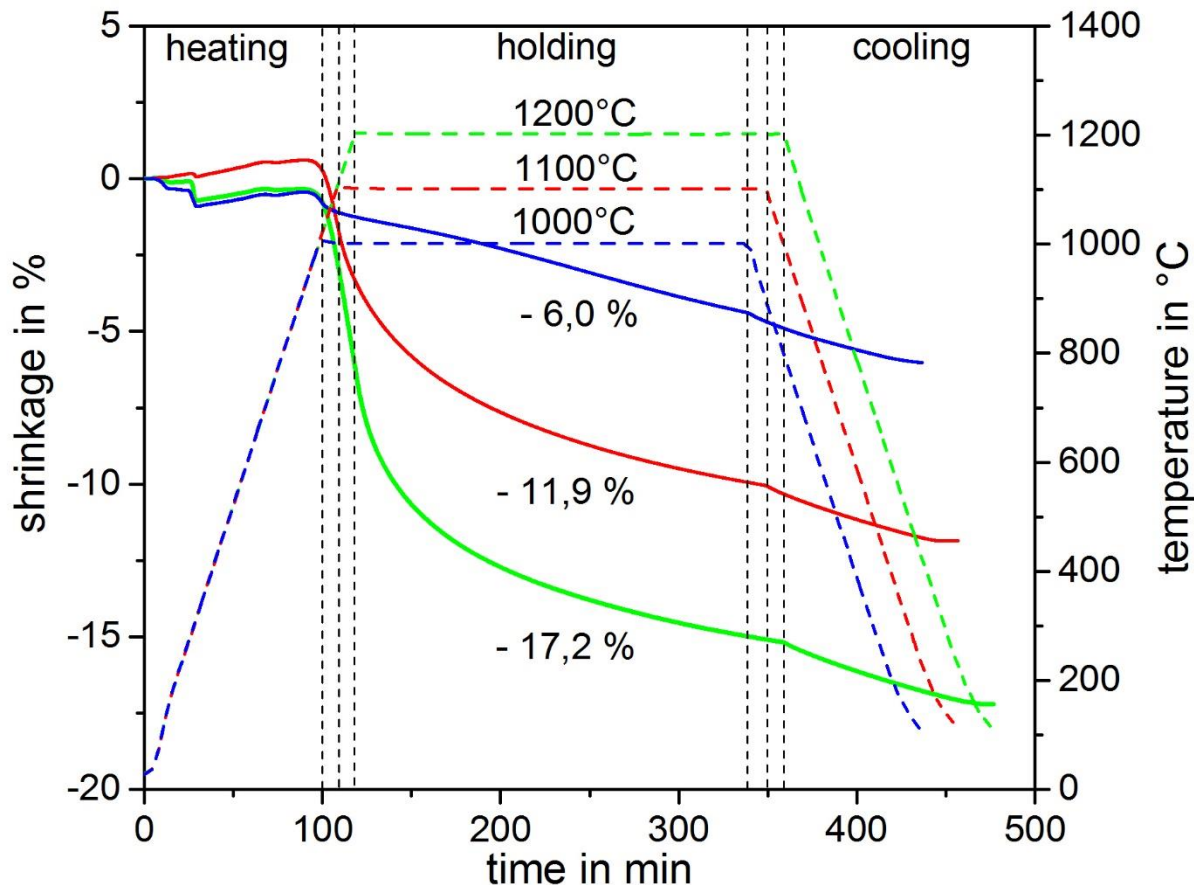
3. Pressureless Sintering (MIM)

Sedimentation Process

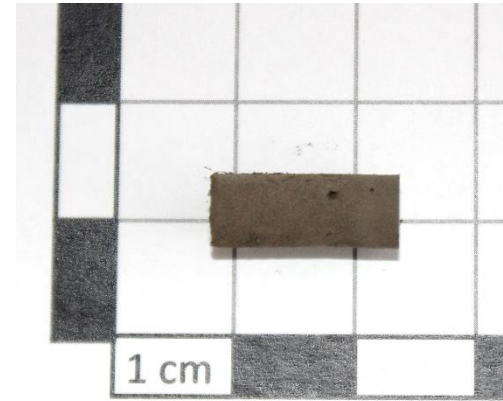


3. Pressureless Sintering (MIM)

Dilatometry of Sedimentation Samples



Results of dilatometry at different holding temperatures
(10 K/min, 4 h)



resulting sample

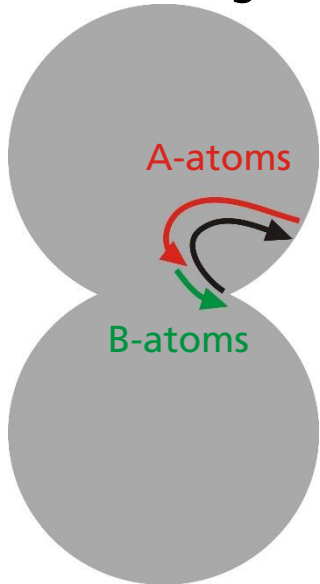
- Usage of smallest powder fractions
- Considerable shrinkage detected
- "Jump" during heating due to debinding of powder
- Debinding finished at 600°C

3. Pressureless Sintering (MIM)

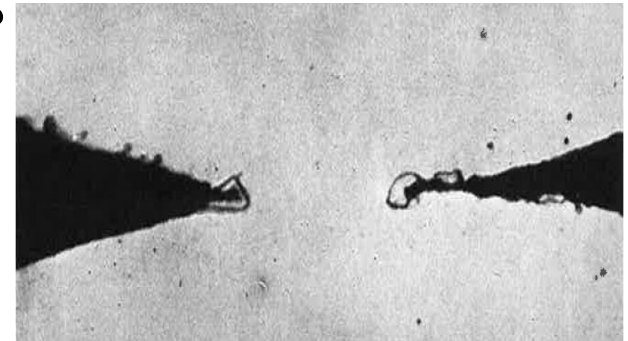
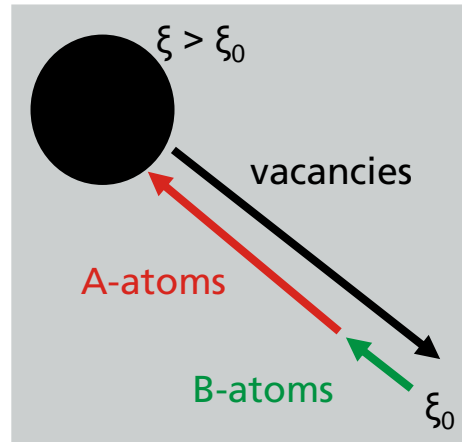
Sintering of Homogeneous Solid Solutions

Homogeneous solid solution A_xB_y ($D_A \gg D_B$)

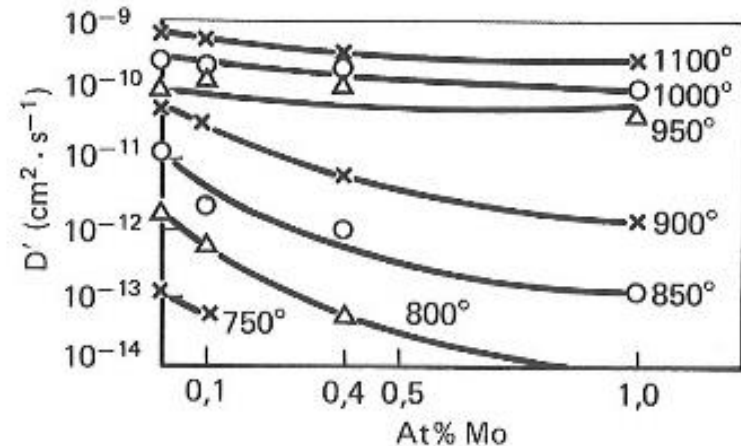
Initial stage



Final stage



Etched neck region between two Cu-wires with 8 at% In [10]

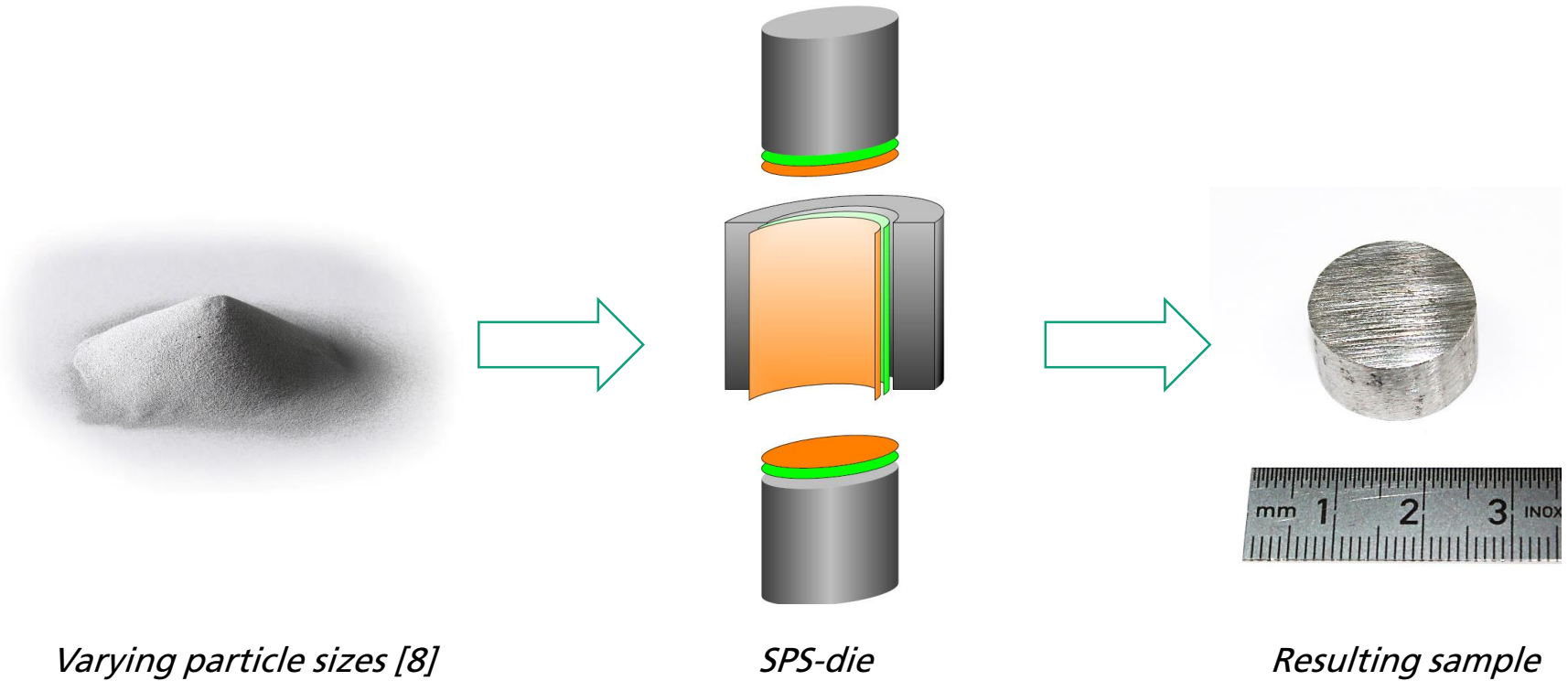


Influence of alloy composition in Fe-Mo alloys on mobility coefficient D' [11]

$$c_A(R) = c_A^0 \left[1 - \frac{D_B}{D_B \cdot c_A + D_A \cdot c_B} \Delta \xi \right]_{r=R}$$

$$\Delta c_A \Big|_{r=R} = c_A(R) - c_A^0 = - \frac{c_A^0 D_B}{D_B \cdot c_A + D_A \cdot c_B} \Delta \xi \Big|_{r=R}$$

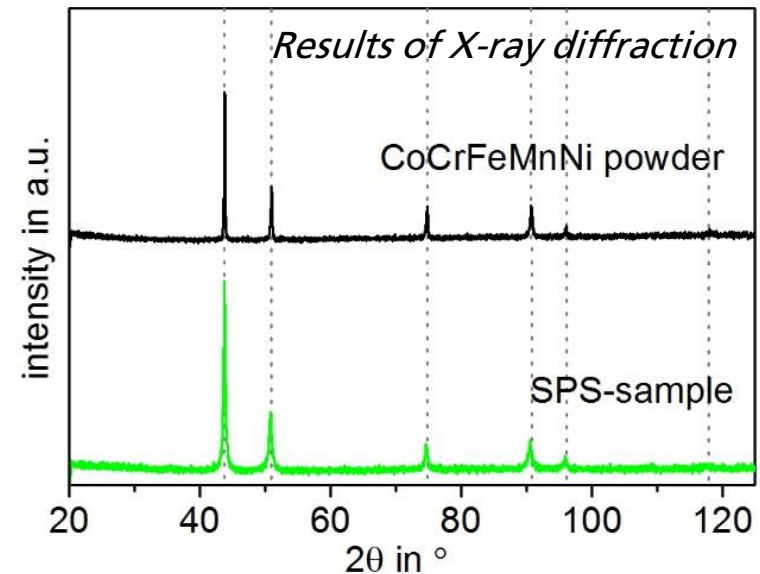
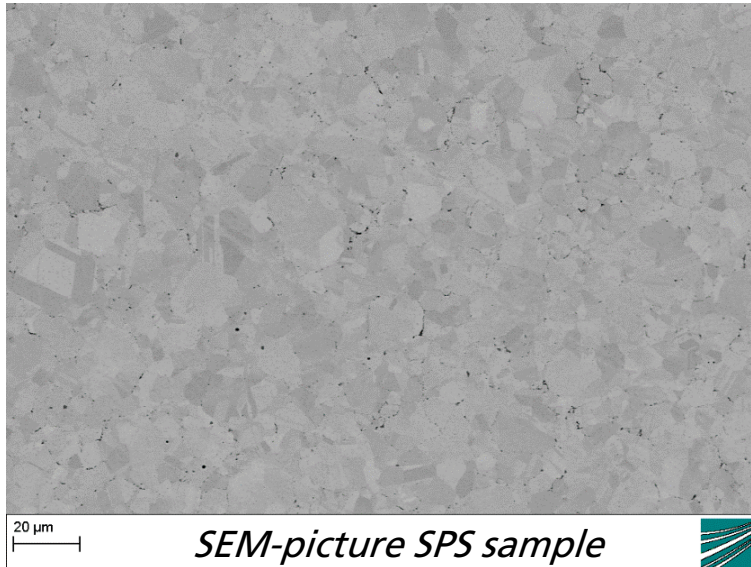
4. Spark Plasma Sintering (SPS)



- Varying particle sizes
- SPS at 1000°C, 55 MPa, Ø 20-30 mm for 10 min
- Application of graphite and tungsten foil

4. Spark Plasma Sintering (SPS)

Microstructure Characterisation



EDS-analysis powder

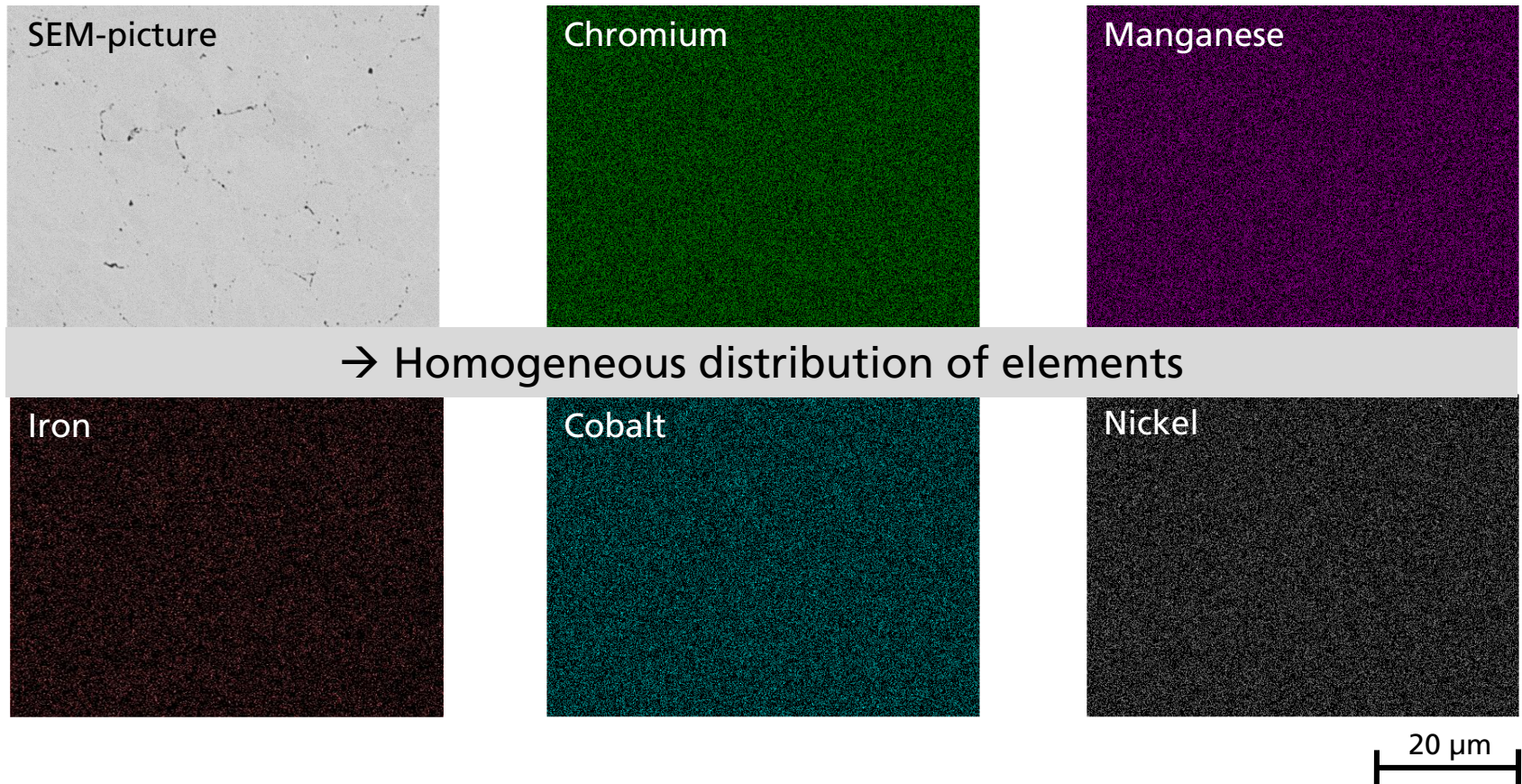
| at-% | Cr | Mn | Fe | Co | Ni |
|---------------|------|------|------|------|------|
| Pulver | 20,2 | 20,2 | 19,7 | 19,8 | 20,1 |
| SPS-Probe | 20,3 | 19,7 | 20,0 | 20,1 | 19,9 |
| He et al. [5] | 21,3 | 20,7 | 19,4 | 19,3 | 19,3 |
| SOLL | 20 | 20 | 20 | 20 | 20 |

SPS sample

- Ideal composition
- Single phase microstructure

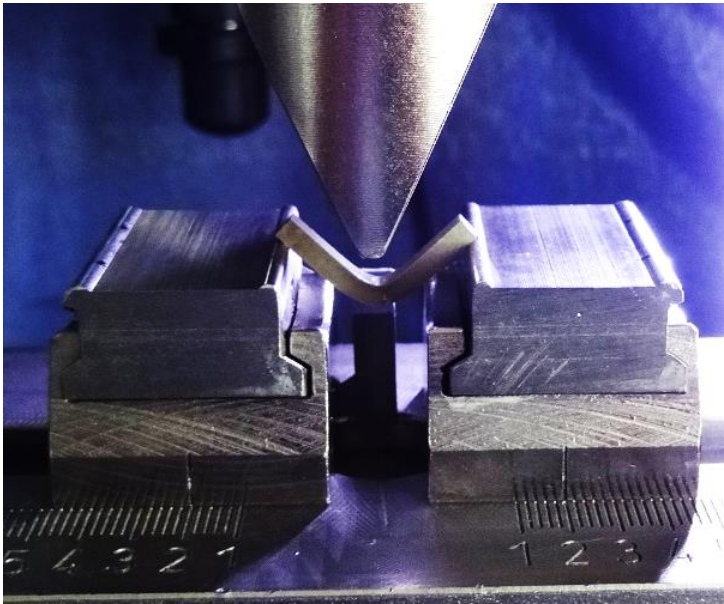
4. Spark Plasma Sintering (SPS)

EDS-Mapping



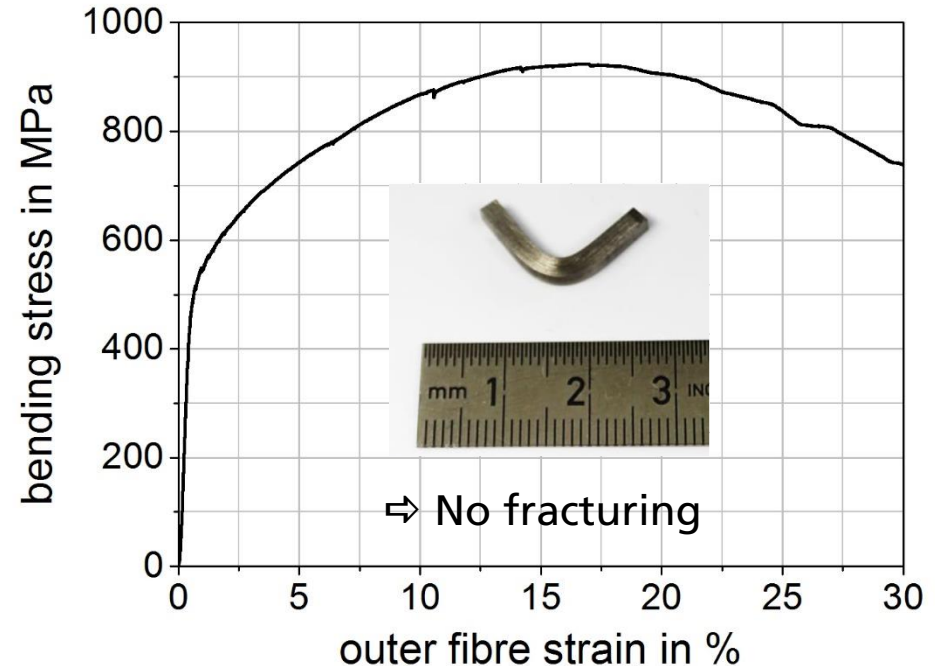
4. Spark Plasma Sintering (SPS)

Mechanical Properties - 3-Point-Bending Test



Testing facility

Bending test:
(25 mm x 2,5 mm x 2,5 mm)



Results 3-point-bending test

- Outer fibre strain at F_{\max} : 16,18 %
- Max. outer fibre strain : > 30 %
- Bending strength: 920 MPa

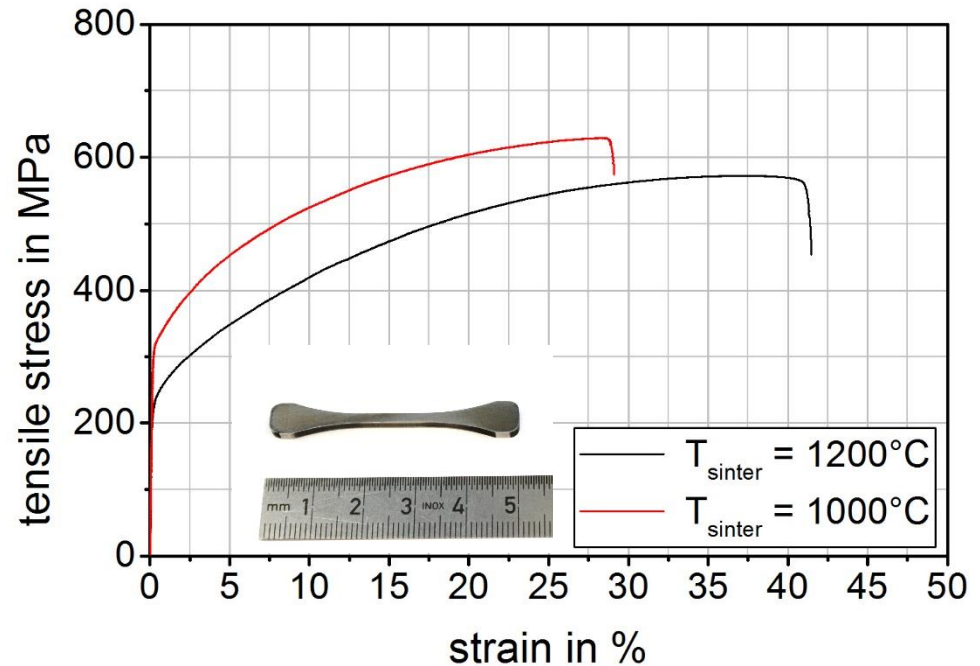
4. Spark Plasma Sintering (SPS)

Mechanical Properties - Tensile Test



Testing facility

Tensile testing:
(50 mm x 2,5 mm x 2 mm)

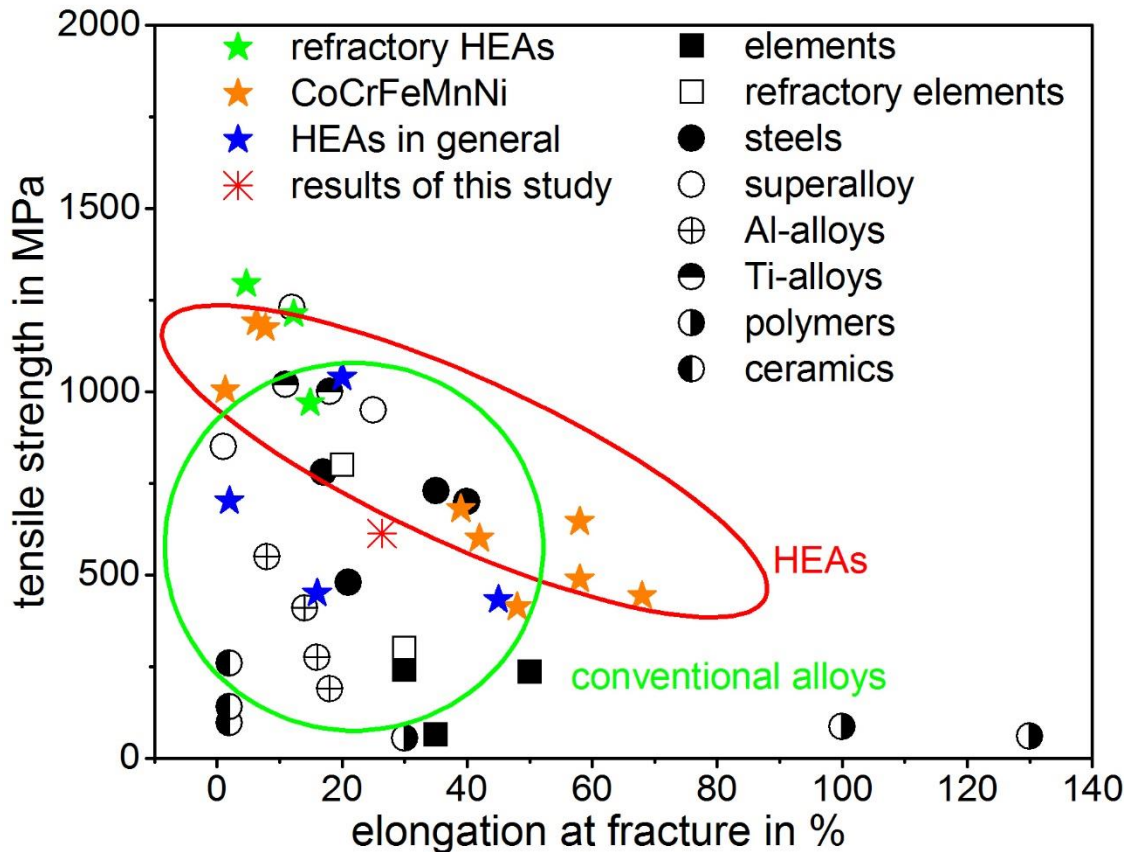


Results tensile test

- Yield strength: 310 MPa
- Tensile strength: 610 MPa
- Elongation at fracture: 27 %

4. Spark Plasma Sintering (SPS)

Mechanical Properties - Summary



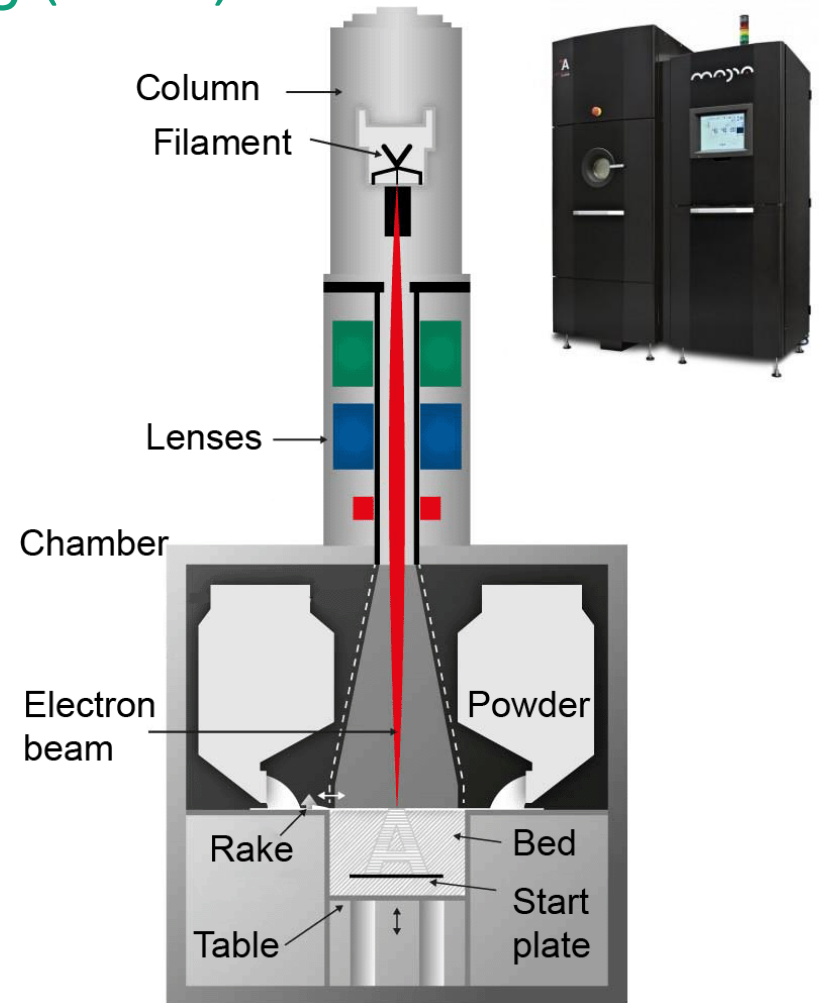
- HEAs can show superior mechanical properties than conventional alloys
- Results of this study fit literature values

Stress-strain- diagram for various conventional materials and HEAs [12-43]

5. Selective Electron Beam Melting (SEBM)

Principles and Basics

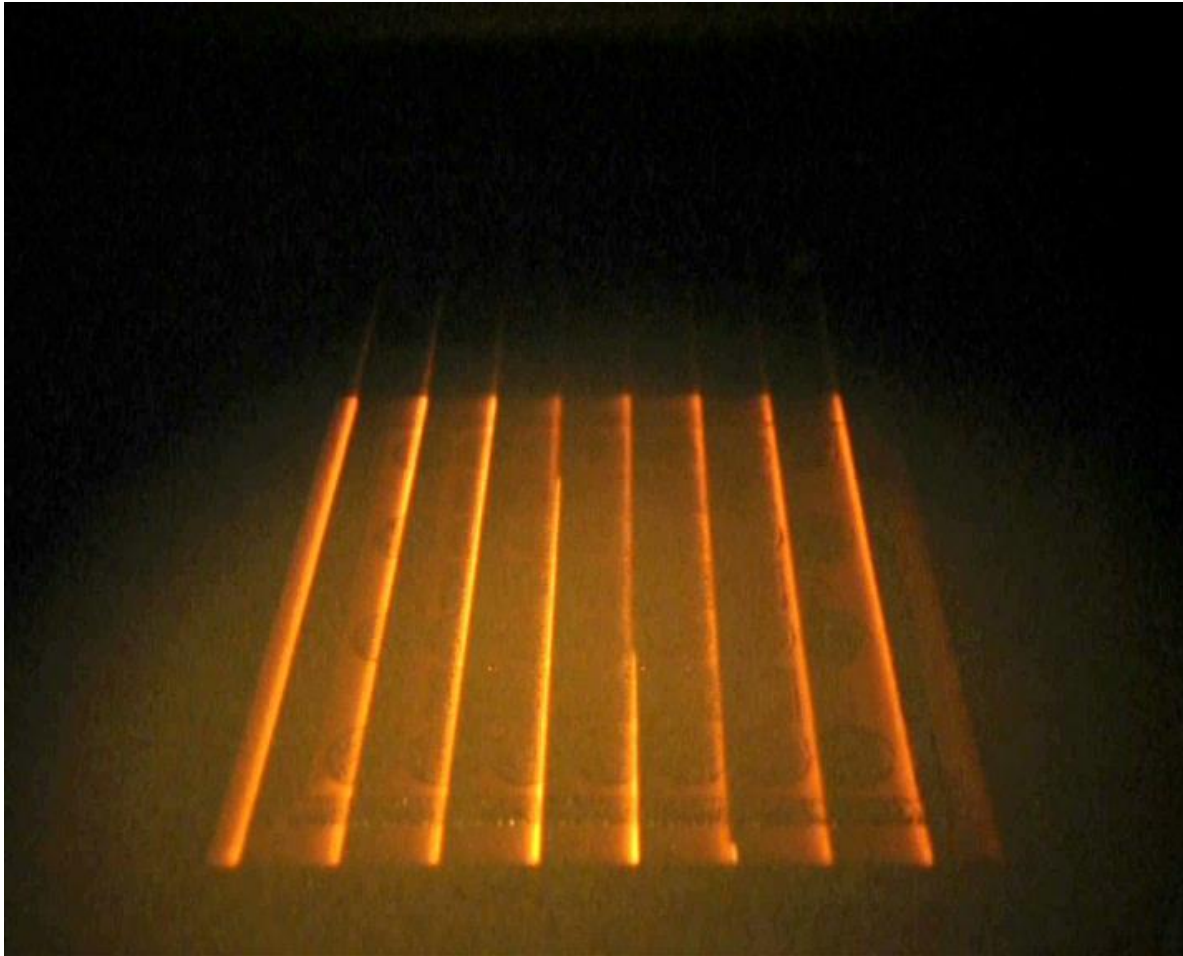
- Powder-bed-based technique
- High beam power
 - ⇒ High-melting materials
- Fast beam deflection
 - ⇒ High building rates
- Vacuum
 - ⇒ Reactive materials
- Pre-heating of powder bed
 - ⇒ Minimising of thermal stresses
 - ⇒ Few supporting structures



SEBM principle und EBM-Anlage [44, 45]

5. Selective Electron Beam Melting (SEBM)

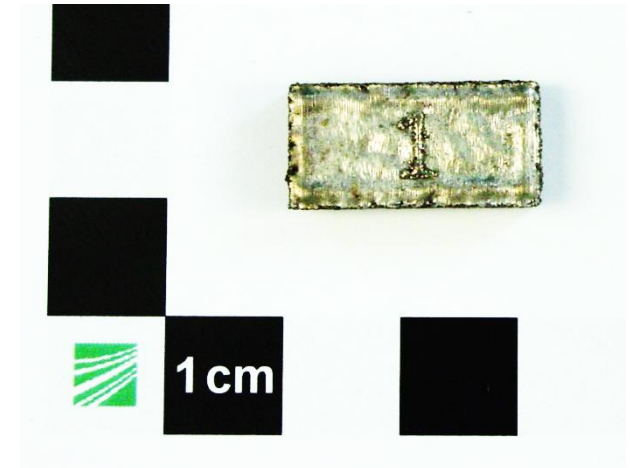
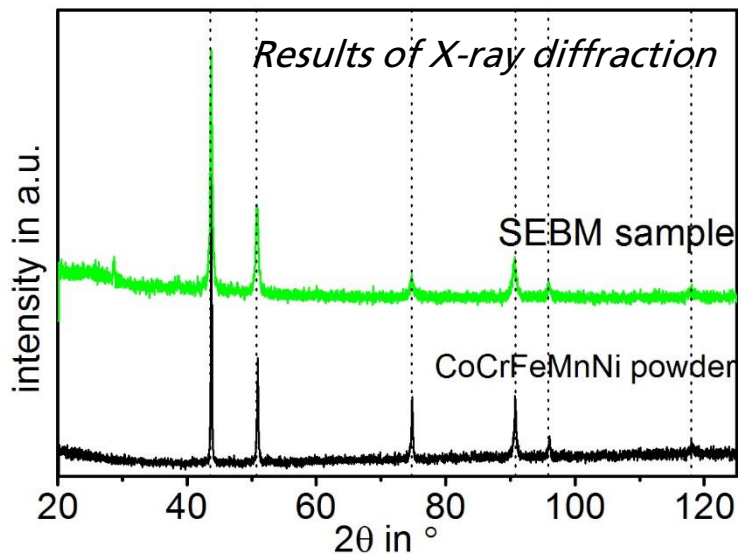
SEBM-Process



5. Selective Electron Beam Melting (SEBM)

SEBM-Samples

- Evaporation of manganese (up to 2 m%)
 - ⇒ No change in crystal structure
- Resulting density up to $\rho \approx 97\%$
 - ⇒ Depending on final composition



HEA-SEBM-samples

5. Selective Electron Beam Melting (SEBM)

SEBM-Microstructure



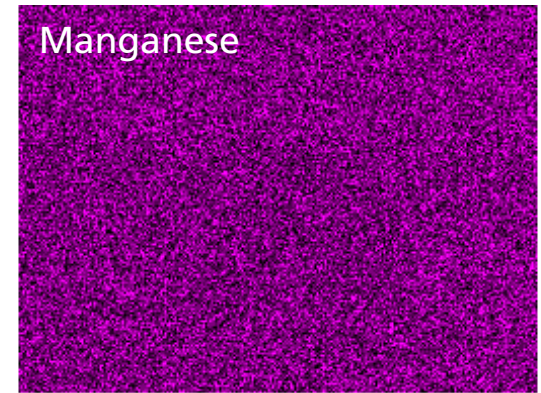
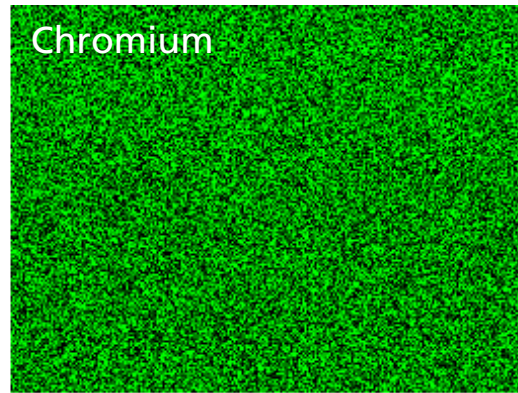
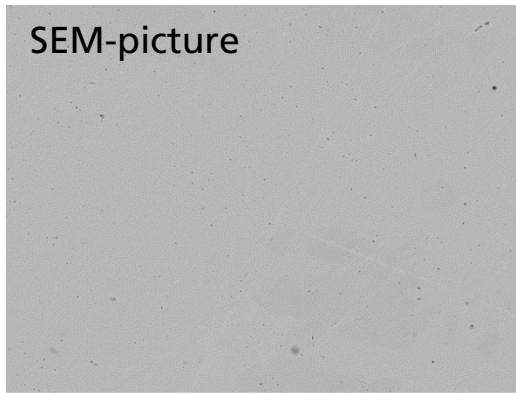
| at-% | Cr | Mn | Fe | Co | Ni |
|---------------|------|------|------|------|------|
| powder | 20,2 | 20,2 | 19,7 | 19,8 | 20,1 |
| EBM | 20,4 | 18,7 | 20,1 | 20,3 | 20,5 |
| He et al. [5] | 21,3 | 20,7 | 19,4 | 19,3 | 19,3 |
| SOLL | 20 | 20 | 20 | 20 | 20 |

EBM sample

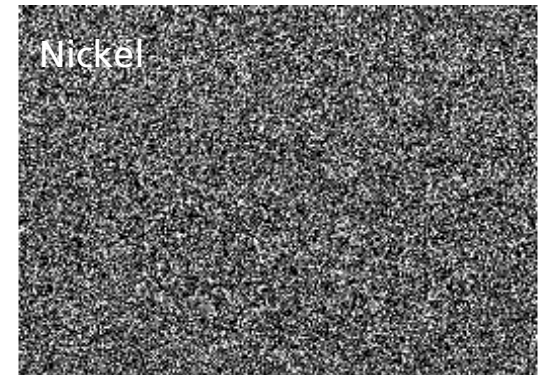
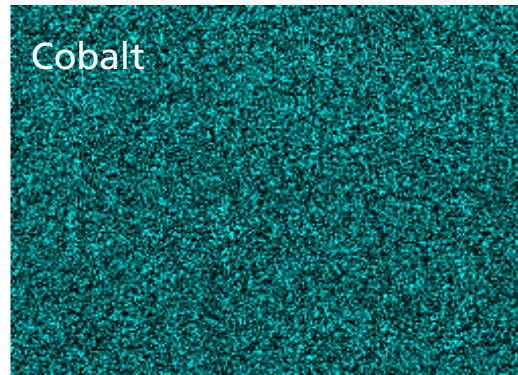
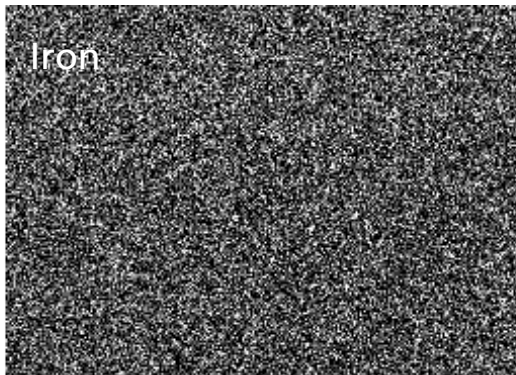
- Composition: Mn deviation (evaporation)
- Single phase microstructure

5. Selective Electron Beam Melting (SEBM)

EDS mapping

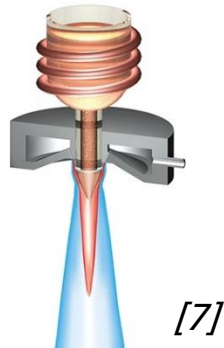


→ Homogeneous distribution of elements



6. Comparison Powder Metallurgical Methods

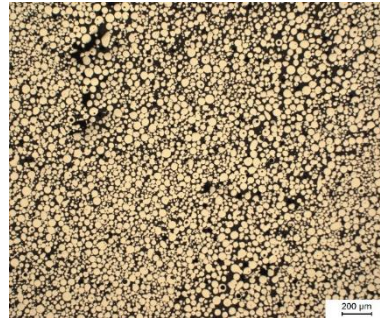
Argon Gas Atomisation



- ✓ Homogeneous and single-phase powders
- ✓ Industrial relevant amount of powder

- Not suitable for all materials and alloys (refractory alloys, etc.)

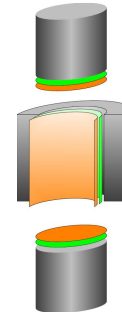
Pressureless Sintering (MIM)



- ✓ Near-net-shape components
- ✓ Analysis of sintering regime

- ↑ Process time

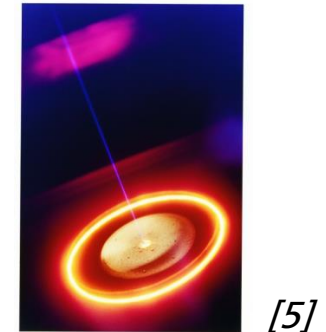
Spark Plasma Sintering



- ✓ ↓ Process time
- ✓ Homogeneous microstructure
- ✓ Density ≈ 99 %

- Limited geometrical possibilities

Selective Electron Beam Melting



- ✓ Complex shapes
- ✓ Homogeneous microstructure
- ✓ Density up to 97%

- ↑ Process time
- Evaporation

7. Summary and outlook

- Powder metallurgy highly suitable for HEA production
- *Powder Production:* gas atomisation
 - ⇒ Homogeneous and spherical powders
 - ⇒ Suitable for industrial application
- *Compaction:*
 - Pressureless Sintering
 - ⇒ Density up to 90%
 - ⇒ No decomposition
 - Spark Plasma Sintering
 - ⇒ Homogeneous and ideal microstructure
 - ⇒ Density up to 99%
 - Electron Beam Melting
 - ⇒ Density up to 97 %
 - ⇒ Evaporation

Thank you for your attention!

References

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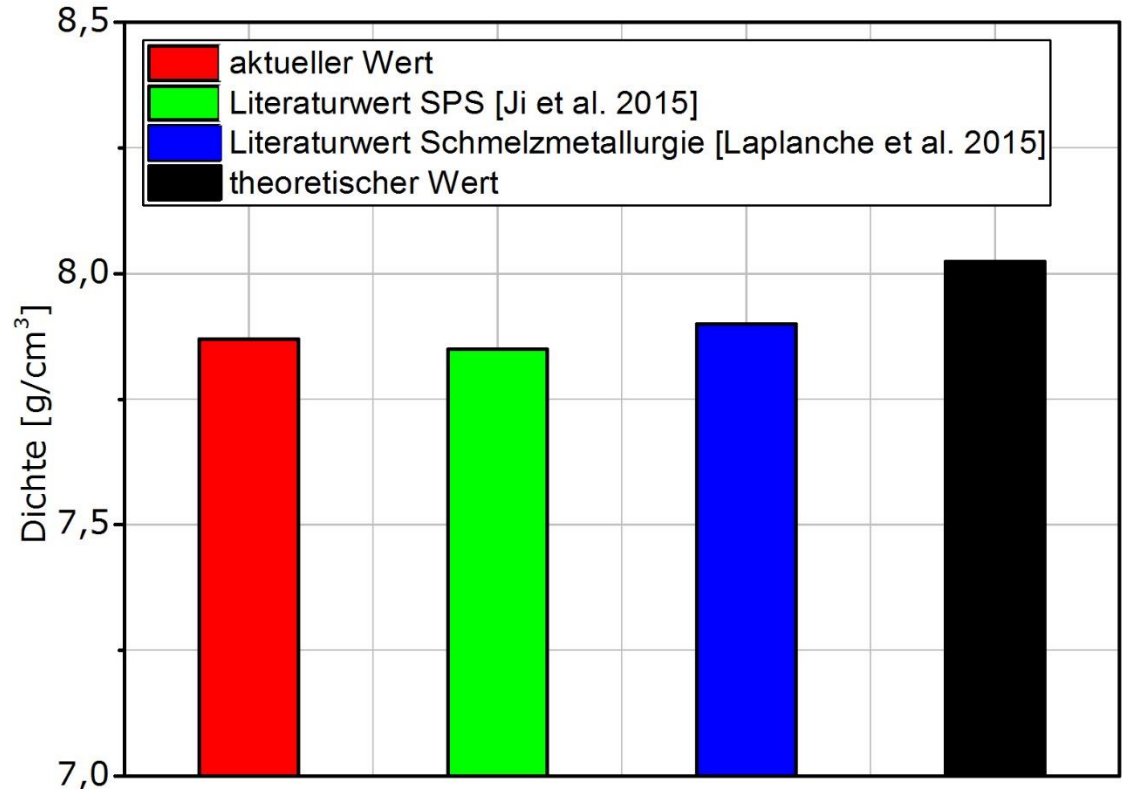
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Appendix

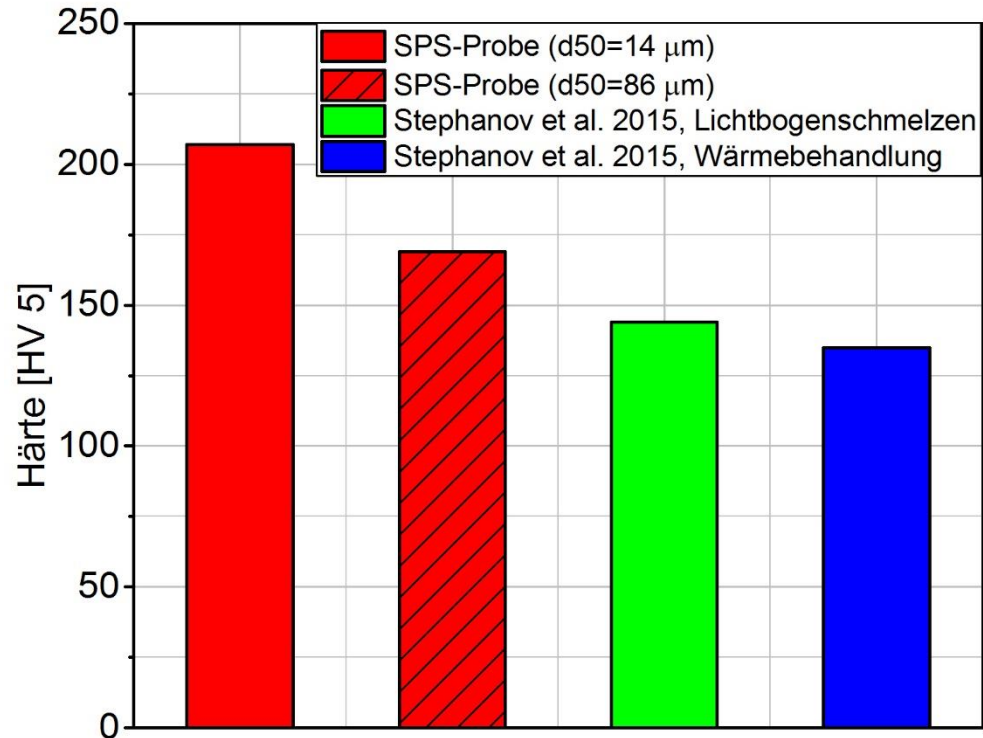
Density of SPS-samples

- Bestimmung mittels Archimedischer Dichtemessung
⇒ $\rho = 98,5 \% \rho_{\text{theor.}}$
- Bestimmung mittels optischer Porenanalyse
⇒ $P = 1 \%$
- Übereinstimmung mit Literaturwerten



Appendix

Hardness of SPS-samples



- Messung der Vickershärte
- ↓ Härtewert bei ↑ Partikelgröße
- Mittels Pulvermetallurgie höhere Härte

$$\Rightarrow HV = 207 HV 5$$

- Wärmebehandlung geringen Einfluss
- Übereinstimmung mit Literaturwerten

Chemical composition

| Probe | | C [m%] | S [m%] | N [m%] | O [m%] | H [m%] |
|----------------|--|--------|--------|--------|--------|--------|
| Pulver | 1. Verdüsung | 0,022 | 0,011 | 0,015 | 0,105 | 0,000 |
| | 1. Verdüsung, 4 Wochen an Luft | | | 0,011 | 0,087 | 0,000 |
| | 2. Verdüsung | 0,022 | 0,007 | 0,016 | 0,062 | 0,000 |
| Fraktion | <32 µm | | | 0,016 | 0,134 | |
| | 32-45 µm | - | - | 0,018 | 0,09 | 0,000 |
| | >160 µm | | | 0,014 | 0,045 | |
| Freies Sintern | Sedimentationsproben | | | 0,034 | 1,16 | 0,099 |
| | Pulverschüttung (<32 µm) 4 h bei 1200 °C | | | 0,004 | 0,079 | 0,002 |
| SPS | <32 µm | 0,215 | 0,008 | 0,018 | 0,123 | - |
| | 63-160 µm | 0,095 | 0,008 | 0,013 | 0,03 | - |